LYSENKO, P.; SHEMYAKIN, I.; GLAZKOVA, P.; SOSHIN, A.; MATTTSIN, P.

Remarkable school of management. Mast. ugl. 7 no. 7:3-8 Jl '58.
(MIRA 11:8)

1. Predsedatel' postoyanno deystvuyushchego proizvodstvennego soveshcheniya shakhty imeni Kalinina tresta Prokop'yevskugol'(for Lysenko), 2. Predsedatel' shakhtnogo komiteta shakhty imeni Kalinina tresta Prokop'yevskugol'(for Shemyakin), 3, Predsedatel' postoyanno deystvuyushchego proizvodstvennogo soveshcheniya shakhty "Koksovaya-1" imeni Stalina tresta Stalinugol'(for Glazkov).

4. Predsedatel' postoyanno deystvuyushchego proizvodstvennogo soveshcheniya shakhty No.4-5 tresta Prokop'yevskugol'(for Sosnia).
5. Sekretar' gorkoma profsoyuza rabochikh ugol'noy promyshlennosti g. Stalina (for Matytsin).

(Mine management)

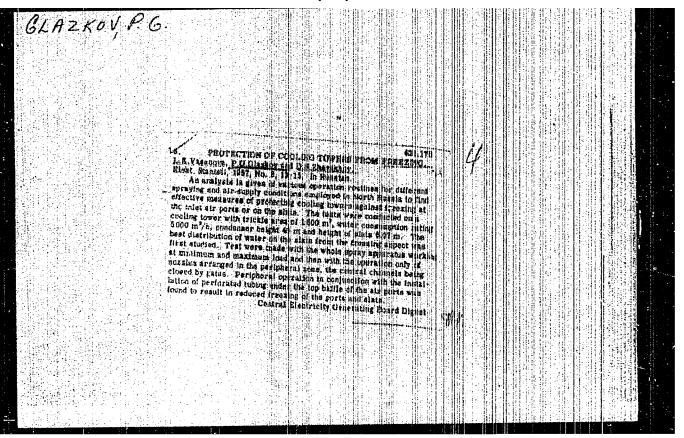
(Cosl mines and canagement)

NESTERENKO, Semen Leont'yevich; GLAZKOV, P.C., inzh., retsenzent;
SERDYUK, V.K., inzh., red.; LTRIUTA, W.A., tekhn.red.

[Instructions on safety techniques for foundrymen pouring metal into molds] Pamiatka po tekhnike bezopasnosti dlia zalivshchikov form metallom. Kiev, Gos. nauchno-tekhn.

izd-vo mashinostroit.lit-ry, 1956. 33 p. (HIRA 12:9)

(Founding--Safety mensures)



183-1-4/24

Glazkov, P.G., Dunayev, N.Ye., Kuzub, A.G., and Panev, G.A. AUTHORS:

The Production of Low-manganese Pig Using Krivoy Rog Ores TITLE:

and Donets Coke (Vyplavka malomar, antsovistogo chu, una na

Krivorozhskikh rudakh i Donetskom Koase)

Stal', 1958, no.1, pp. 14 - 20 (USSR). PERIODICAL:

GLAZKO

Transfer of the blast furnaces on the above works to the ABSTRACT: production of pig iron with a sampaness content of about 0.8 -0.9% (as against 1.9% previously produced) is escribed. The decrease in manganese content was carried out in stages with simultaneous increase in slag basicity (CaO/SiO2 about 1.3)

and alumina content of slag (to about 10%) without encountering any operational difficulties. Chemical composition of raw materials is given in Table 1. Furnace-operating data - Tables 2 and 3. The dependence of sulphur content in pig on manganese content at various levels of silicon content - Fig. 1. The average monthly composition of iron and slag - Table 4. The dependence of sulphur content in pig on slag basicity - Fig. 5. It is concluded that under works' operating conditions, the transfer of furnaces to the production of low-manyanese pib increased the output of iron by 5-6%, decreased the coke rate by 6.5%, decreased the consumption of manganese ore by 73.5% and

Cardl/2 increased the consumption of fluxes by 6.72%. The cost of

The Production of Low-manganese Pig Using Krivcy Rog Ores and Donets Coke

production of pig iron decreased by 5.18%. There are 4 tables, 5 figures and 7 Russian references.

ASSOCIATION: Stalino Metallurgical Works (Stalinskiy metallurgich-

eskiy zavod)

AVAILABLE: Library of Congress

Card 2/2

Carry Mary To

133-58-5-0/29

AUTHORS: Glazkov, P.G., Ofen andre, A.M., Drunki, G., I.I.,

Nesterovich, R.F. and Clepurnoy, G.T., Beginsens

TITLE:

Smelting of Steel from Low Langanese Iron (Wyslavice Divili

iz malomargantsovistogo chuguna)

Stal', 1953, Hr 2, pp 209 - 213 (USJA) PERIODICAL:

The influence of low-manganese from our the operation of ABSTRACT:

open-hearth furnaces and the quality of the motel produced was carried out by a comparative abudy of the individual opening factors for heats in thich lon-man amove from (250 heats) and normal iron (232 heats) were used. Heats carried but on the same furnace were usually compared. Low-manganese inpares poured directly into open-hearth furmices while normal iron for about 40% of heats was passed through a nixer. Salli of steel was carried out by the scrap-ore process in 130-tor open-legath furnaces with ma nesite chromite roofs, fired with a mixture of coke-oven and blest furnace (as. Due to the light a ligher content in the color oven pas (13-15 1/m²) a considerable amount of limestone was used in the clarate content as the content of the color over the clarate content as the clara of limestone was used in the clarge, about 90 a /bon of ficished steel. During smelting slag was changed twice during the melting and refining periods with subdecuent varia, of fresh slag by time additions. Peats were into sive end out sitt who

Cardl/4

Smelting of Steel from Low Manganese Iron

133-58-3-6/29

reduction of manganese, the content of which during one boiling was not controlled. Chemical composition of low-manganese pig: % Si 0.79, Ma 0.91, 3 0.034 and that of mountaing: % Si 0.78, Mm 1.25, Si 0.046 (Fig. 1). For greater distribution of the sampanese content after melting (A) and tefore decordation (B) - Fig. 2; charges in the stag composition during smelting with low-manganese pig (nominator) and ordinary pig comelting with low-manganese pig (nominator) and ordinary pig the finished metal - Fig. 3; the dependence of the subject content in the metal after melting on the subject exacts of the pig - Fig.4; the dependence of subplur content is actal after melting on the duration of dright and heating of the charge - Fig.5; the dependence of the velocity of describing action and subplur content at the beginning of boiling on subplur content of metal after melting - Fig.6; frequency distributions of phosphorus during various smelting low-manganese insulation of materials and related to 1t, the cost of production of steel - Table 2. Conclusions: The content of production of steel - Table 2. Conclusions: The content of manganese in motal during the finishin priod in leater its low-manganese pig was lower by 0.00-0.003 than that he is a little the usual pig, although the transfer of manganese from clarge.

Smeltin, of Steel from Low Manganese Iron 133-50-3-6/29

to metal was increased from 31.8 to 425. Or transfer to hermanganese gig, the condition for the desulphraisative of the metal bath deteriorated and the content of colphur in metal after melt but increased on everye by 0.004%. This led to a prolon ation of the finishing period and an ar menicately 15 decrease in the origid of open-harth furnaces. The production of metal with a required low sulphur content becomes here difficult. In heats with low-came anese win, the content of sulphur in metal after the nelt out increases with increasing sulphur content of sic, while with the nough ic, its sulphur content up to 0.05% has so influence on the sulphur content of metal after the holt out. The transfer to low-many among sign had no influence on desulphurisation of the bath during refining, on the removal of phosphorus and on the modeso of slag formation, but the yield of good metal incremed by 0.3%, the consumption of ore decreased by 0.75 kg/ton of steel and the amount of ferro-man ancie used for decalidation increased by like/ton of stell. The quality of steel promocd from lowmanganese pig did not deteriorate while the raduction costs somewhat decreased (by 11.62 roubles/ton). The applier tion of low-manganese pig for the production of steel would be effective Card 3/4

Smelting of Speed from Low Mangarese Iron

133-50-3-6/29

if coke even was used for firing was desulphusised. There are 2 tables and ? Figures and ? Soviet inferences.

ASSOCIATIOn: Spole mkiy metalburgicleskiy nevod (Staling Tital metalburgical Morks)

AVAILABLE:

Library of Con reso

Card 4/4

307/137-59-5-9809

Translation from: Referativnyy zhurnal, Metallurgiya, 1959, Nr 5, p 47 (UCSR)

AUTHOR.

Glazkov, P.G.

TITLE:

Smelting and Reduction of Low-Manganous Cast Iron

PERIODICAL.

Byul, tekhn, -ekon, inform, Sovnarkhoz Stalinskogo ekon, adm

r-na, 1958, Nr 5, pp 17 - 21

ABSTRACT -

The author presents results of a new technology for the smelting and reduction of low-manganous cast iron brought into use at the Stalino Metallurgical Plant on the basis of experience made at Eastern USSR plants and also of experiments carried out at the Flant during 1956 - 57. The basic factors in the new technology were the changes in the slag process and high heating up of the hearth; slag basicity was brought to 1.28 - 1.30, with 7 + 10.6 Al $_2$ 03 and 3 - 4% MgO content. The cast iron temperature at the moment of tapping was 1,460° - 1,500°C. As a result, when Mn-ora was fully removed from the charge of blast furnate Nr 3, its

Card 1/2

smooth operation was not impaired; efficiency was raised by 5 - 6%, sost price of the cast from was reduced by 6 - $7.6 \cdot [5]$

807/137-59-5-9809

Smelting and Reduction of Low-Manganous Cast Iron

content in the cast iron decreased by a factor of 1.5 - 1.8, [Mn] did not exceed 0.2%, Si did practically not change. To determine the efficiency of open-hearth reduction of low-manganous cast iron, 222 smelts were carried out at the Plant with conventional cast iron and 287 smelts were made with low-manganous east-iron containing on the average 0.91% Mn, i.e., half as high as the conventional amount (1.86%); the S content was diminished by 1.2 - 1.5 times in comparison to the conventional amount In low-manganous cast-iron reduction the consumption of Fe-ore decreased on the average by 1 ton per smelt (7 - 7.5 kg/t of steel). Duration of the smelt was shortened by 0.08 hours (in operation with unpurified coke gas). [3] in the steel did practically not change but the desulfurization rate during the polishing period increased from 0.005 to 0.007% per one hour. As a result 60% of S eliminated during the finishing stage departed from the metal during the time of clean bubbling. The Fe-Mn consumption for deoxidizing and alloying increased on the average by 1.1 kg/t of steel. A total economy of 11.62 rubles per 1 ton of steel was attained with the use of low manganous cast iron.

G.Ch.

Card 2/2

Glazkov, F.G. AUTHOR:

307/130-75-6-1/20

TITIE:

Alon, the Path of Technical Progress (Po puti tekhnici askaga

progressa)

PERIODICAL: Metallurg, 1958, nr 6, pp 1 - 2 (USSR).

ABSTRACT: The authorstates that production at the Stalino Metallurgical works has been prestly increased since 1940 with substantially the same number of units by following a technically progressive policy and elevating the creasive activity of workers and engineers. he gives examples of developments in which the works has led, including: evaporative cooling of open-hearth and blast furnaces and the production of lowmanganese, low sulphur (under 0.040%) pig iron in the south. The low-manganese iron is smelted with a slag basicity of at least 1.30, a silicon content in the iron of at least 0.65, at least 7% Al₂O₃ in the slac and with at least 30% of the total

flux as dolomitized limestone. The central works laboratory have established a relation between relial carbon disyide distribution in the blast furnace throat and top-jas temperature and the latter is now used for process control. A special redicactive level-moter has been developed at the larks to enable dust losses from the blast farm on to be found enable Cardly3

Along the Path to Technical Progress

007/130-58-6-1/20

and this is undergoing works tests. In the melting shop, open-hearth furnace roof construction was improved in 1957 and dimab-chromite bricks have been used in the upper checker levels; how-corbon steels have been produced without oreliminary destricted in the furnace and the mounts of aluminium for droxidial a layer been reduced; laget weights have been increased, anothing papers of rolled products to be raised by 3.10; see itsels, including type 25.3 for-alloy reinforcing, have been produced; radioactive instance are widely used for steel-malting layestic tions. In the rolling mills reconstruction, automation, mechanisation and improved pass design have been advantageously carried out, one of the examples given by the author being the adoption of fluted rolls in the three-high stand of the sheet mill. The author names the following works' personnel as being among those who have contributed useful inventions: Disho, Dubchenko, Oleksa, Kotov and Rovtorin. He states that savings through su jections adopted in 1957 are about 4 million roubles. At present, a large,

Along the Path of Technical Progress

SCV/130-58-6-1/20

continuous-casting installation is being built in the melting shop, and a large heat-treatment shop is to be built shortly. Research work is continuing.

ASSOCIATION: Stalinskiy metalturgicheskiy ravoč (Stalino Petallurgical Works)

Card 3/3

1. Industrial plant - USSR 2. Motallurgy - Development

18.3200

307, 11 1 1 1 1 1 2 2 7 7 2

AUTHORS:

Belov, I. V. (Candidate of Terminia, Date 1987). Vilinganskip, I. No., Annae Joseph K. J. Royalle, P. Ye., Telepon, J. A., persona S. J. (Socialis).

TITLE:

Delivery of Air to the roots of Post of Establish the

Melting Process

PERIODICAL:

Staff, Iron, Killing of the or (Mask)

ABSTRACT:

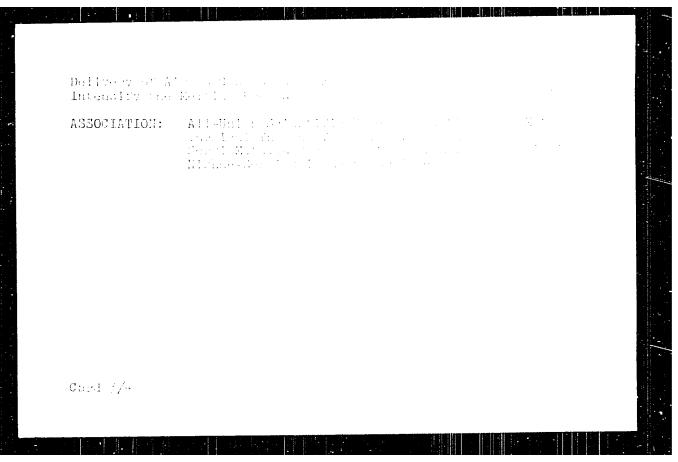
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Card 1/4

Delivery of Air to Gad Porth of Pincip Intensity the Melting Process

derap-ore process with diplicated her and active coke-over gas fired. I who will not her all active compare the new and temperative when the sine of compare the new and the self-based of the sine of table). The following employer at the self-based of the self-base

Card 2/4



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2. **	Bacls Pendomarks of Fig. 5. 5. 5 Without Course to the Listing by Par	ndin in heli Ta	! :	
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	en Theresi Load sandik Stalyh			
Fu	unace Projectiviti. 1, 1, 1			
Art	bitomory Pack Compute the Zu ed 4/2	•	•	

9/137/62/000/001/014/237 A060/A101

AUTHORS:

Glazkov, F. G., Sladkoshteyev, V. T., Telesov, S. A., Ofengenden,

A. M., Strelets, V. M., Murzov, K. P.

TITLE:

Study of the operation of a multi-jet casting unit for continuous

pouring of steel

PERIODICAL: Referativnyy zhurnal, Metallurgiya, no. 1, 1962, 62, abstract 1V392

("Sb. tr. Ukr. n.-1. in-t metallov", 1961, no. 7, 133-142)

On the basis of temperature measurements of steel in the furnace, TEXT: in the ladle of 140-ton capacity, and also in a 2-stopper intermediate casting unit, and in the jets from the ladle and the casting unit, the heat losses of molten steel in the process of tapping and founding were determined. It was established that the first 18 - 20 tons of steel proceeding from the ladle and the casting unit have a relatively low temperature, which then increases and remains stable practically to the end of the founding. Taking into account that the low temperature of the first portions of the metal is the result of heat losses expended upon the heating up of the lining of the ladle and the casting unit and leads to a rapid obstruction of the channels of the steel-pouring

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Study of the operation of a multi-jet ...

S/137/62/000/001/014/237 A060/A101

nozzles, it is recommended to heat up the working layer of the lining up to 1,300 - 1,400°C. It is indicated that the raising of the lining temperature of the casting-unit lining between the limits 1,000 - 1,350 C reduces the steel temperature drop by 8 - 10 C per 100 C lining temperature increase. It is pointed out that the total obstruction of the nozzle channels is eliminated at the temperature of molten rimmed and killed (medium-carbon) steel in the furnace before tapping and in the casting unit (after pouring 3-6 tons), equal to 1,625 - 1,650 and 1,530 - 1,550°3 respectively. Testing was carried out upon the composite nozzles of fireclay with zirconium, high-alumina, and magnezite bushings, and also upon biceramic ones with argillo-graphite and high-alumina working layer. It was established that in the course of pouring rimmed steel the lowest channel erosion and the most stable metal flow is ensured by highalumina and zirechium bushings. In pouring killed steel it was established that the method of raducing the steel with Al has an effect upon the nature of steel action upon the nozzle material. In pouring steel reduced with Al during tapping the heat, the nozzle channel becomes stopped up in the course of pouring and requires repeated burning out with $\mathcal{O}_{\mathcal{O}}$. However, also in that case the best result is obtained with a zirconium bushing. In reducing killed steel with Al the most stable flow of metal in the jet from the casting unit was demonstrated

Card 2/3

Study of the operation of a multi-jet ...

S/137/62/000/001/014/237 A060/A101

by zirconium and high-alumina bushings. Computational formulae are given for determining the channel diameter of the nozzle in the casting unit, which ensures a given flow of rimmed or killed steel.

I. Granat

[Abstracter's note: Complete translation]

Card 3/3

GLAZEDY, P.G., inzh.; SLADEOSHTSYEV, V.T., kand.tekhn.nauk; TELESOV, S...,
inzh.; OFENGENDEN, A.M., inzh.; Challeft, T.E., kand.tekhn.nauk;
I.T.; TELLSOF, A.V.; YEVILSHEMPY, V.B.; MALAFRA, A.V.; DROFFETM,
YU.Z.; SLIN'KO, A.N.; ZELENDY, S.M.; GENFLY, V.G.; BHASKLI,
YYSOTSFAYA, T.E.

Investigating the operation of multiple-pit mountains steel cesting arrangements. Truny tkr. naush.misl.inst. mat. nau.9:133-142
(Kita 14:11)

(Continuous casting--Equipment and samples)

d/130/62/000/011/001/012 A006/4101

AUTHORG:

Glazkov, P. G., Chief Engineer, Murzov, K. P., Deputy Chief of the pen-hearth shop for continuous steel casting, Koniratyuk, A. M., Deputy Chief of the continuous steel casting equipment

TITLE:

Two-year experiments on continuous steel easting

PERIODICAL:

Metallurg, no. 11, 1962, 19 - 31

TEXT: A four-machine unit for continuous steel casting has been operating for two years at the Denetskiy metallurgicheskiy zavod (Conets Metallurgical Plant). The machine is intended for casting slabs of 120 x 300 to 200 x 1,000 mm size. The cast metal is cut into blanks and slabs. The vertical-type unit is 27 meters high. Each of the four machines is equipped with thin-walled 1.5 m high crystallizers. The equipment includes also roll-batteries, drawing stands, gas cutters, devices for the clamping of c u t blank pieces, and for transporting and removing the slabs. Two intermediate 12-ton ladies are sounted ever the crystallizers. At the present the steel on the described unit is cast into crystallizers of 125 x 700; 200 x 800 and 200 x 1,000 mm size with sentral jet supply; optimum metal teeming temperature is 1,620 - 1,640°C, and optimum

Card 1/2

Two year experiments on continuous steel casting

W13W69/000/6:1/c01/00g

temperature of preheating the intermediate latter to 1.15. \pm 1.275. After ϵ nounles on - 20 mm in diameter, with 53 - 5-5 or content and over 1,5000) per fractoriness are used in the intermediate ladles. This is possible due to the selection of proper conditions of metal decordation in the latte, namely using 7 by ferromaganese, 5 by 735 ferro-silic n. 0.3 by aluminus and 1 by ferrotitanium for deoxidizing ! ton of low-carbon killed steels. The erystallinens are relatively durable and withstand 2 - 3 compaigns, with 8.5% bons cant size. per dampaign. Optimus teeming rates are 6.55 - 9.65 symin to 175 - 77 am geotiens, 0.45 - 0.55 π/\min for 200 x 800 sm and 0.5 - 0.5 symin for 150 s 1,000 mm sections. The weight teeming rate for all sections is about 6.7 t/min and teeming time is 55 - 60 min for easting steel from a 140-ton laste. Springs cooling conditions are: 48 m3/h water supply for 200 x 500 cm ingets, and $36 \text{ m}^3/\text{n}$ for 175 x 700 mm ingots. The continuous steel casting techniques make it possible to raise the production volume and to reduce rejects. Further improvements are being developed and concern improved durability of crystallizers, casting of steel with 0.19 - 0.30% C, and casting low-alloyed steels. There

ASSOCIATION: Donetskiy metallurgicheskiy zavod (Donets Metallurgical Plant)

Card 2/2

GLAZKOV, P.G., inzh.; GRIGOR'YEV, F.N., inzh.; MURZOV, K.T., inzh.;

SUMEMOCHTEYEV, V.T., inzh.; Prinimali uchastiye: MALAKHA, A.V.;

POKRASS, L.M.; DRUZHININ, I.I.; OSIPOV, V.G.; KONTRATYUK, A.M.;

POLYAKUV, I.V.; GORDIYENKO, M.S.; PAVLOV, M.T.; KOPYTIN, A.V.;

PARASHCHENKO, R.A.; POTANIN, R.V.; AKHTYRSKIY, V.I.; BRUK, S.M.;

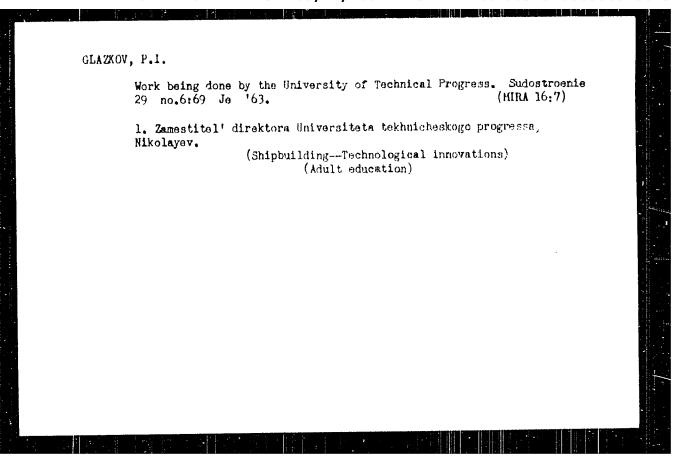
YEVTUSHENKO, V.V.; LEYTES, A.V.; STRELETS, V.M.

Continuous casting of 140-ton steel heats with four-channel equipment, Stalt 20 no. 6:601-504 Je 167. (MIRA 16:7)

ANDON'YEV, SCH., GLAZKOV, P.G. [deceased], KUCHIN, V.A. KONDRAT'YEV, Ye.M.;
LEVITASOV, Ya.M., MAKAROV, K.I., PANKPATOV, I.V.; PEVITY, N.I.;
POKRAS, L.M., FOCHTMAN, A.M.; TENNER, P.A.; SHEYNDAYN, F.I.;
SHKLYAR, T.I.; Prinimali uchastiye: BERMAN, M.N.; VARFALOMEYEV,
F.L.; BOBIN, M.A., MOYSIYEVICH, G.I.: SAPIRO, V.S.; ALEKSEYEV,
L.M.; FOFOVA, R.S.

Heating Martin furnaces with natural gas using reformers.

Gaz. prom. 9 no.11:14-17 104. (MIRA 17:12)



Ri

ACC NR: AP6030241 (AN) SOURCE CODE: UR/0394/66/004/007/0032/0033 AUTHOR: Glazkov, P. N.

ORG: Kazakh Scientific Research Institute of Plant Protection (Kazakhskiy nauchno-issledovateľskiy institut zashchity rasteniy)

EWICL)

TITLE: Phytotoxic effect of vegadex on onion and dodder

L'09122-67

SOURCE: Khimiya v sel'skom khozyaystve, v. 4, no. 7, 1966, 32-33

TOPIC TAGS: vegadex, onion, dodder, grey soil

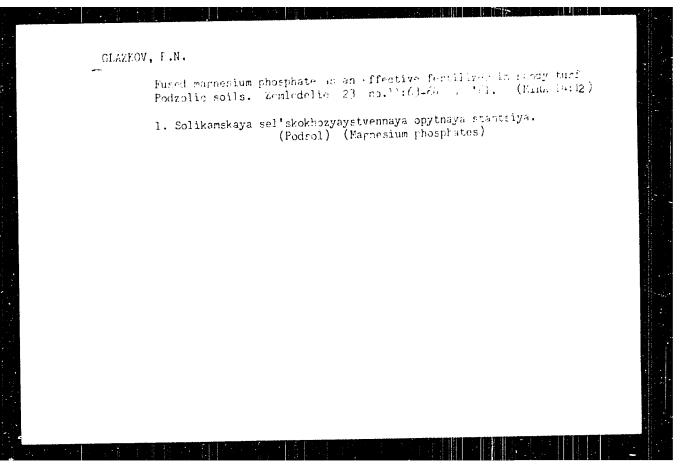
ABSTRACT: In 1964-1965, experiments were made with vegadex (2-chloralil-N, N-dietilditiokarbamat containing 46.7% of o/v in grey soils of Dzhambul Oblast . to find a herbicide for destroying the dodder which is very harmful to onion crops in the irrigated area of Kazakhstan. It was found that spraying of the soil with a 25 kg/ha dose of vegadex (500 l/ha of working solution) before sowing destroyed 94% of the dodder offshoots and sprouts. The thickness of the onion growth decreases by 37--38% at the time of harvesting, yet because the surviving onions develop better, the overall harvest increases 62.8% as compared to the control harvest. Tests made in 1965 showed that if vegadex penetrates the soil to depths

Card 1/2

UDC: 632, 954:635, 25

ACC NR: AP6030241	0
of 1-2 cm, it destroys dodder completely, but also thins the onic 88.694.6%. If vegadex is sprayed on the surface of the soil, 7 dodder is destroyed and thinning of onion offshoots is only 5.4%. is therefore considered to be the best method for destroying dodd has: 2 tables. [w. A. 50]	2.8% of the Surface spraying
SUB CODE: 02, 06, 07, 08/ SUBM DATE: 13Nov65/	
AND CONTRACTOR OF THE STATE OF	

GLAZKOV, P. N., Cand Agr Sci -- (diss) "Effectiveness of varieties of phosphoric fertilizers in grassland crop rotation on light sod-podzolic soils." Moscow, 1960. 18 pp; (State Committee of the Council of Ministers USSR for Chemistry, Scientific Inst of Fertilizers and Insect Fungicides im Ya. V. Samoylov); 250 copies; price not given; (KL, 29-60, 126)

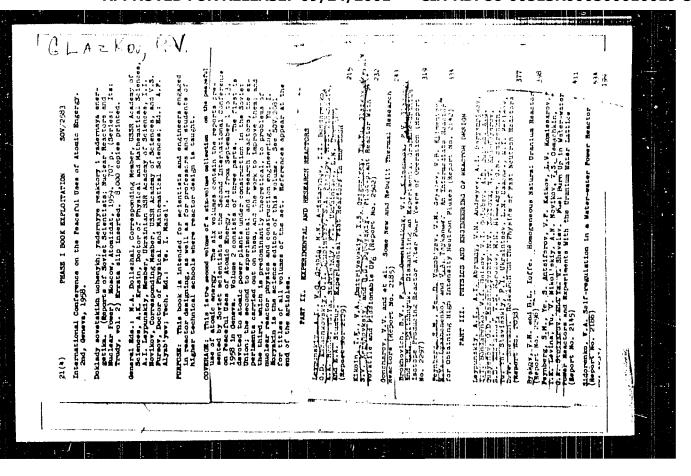


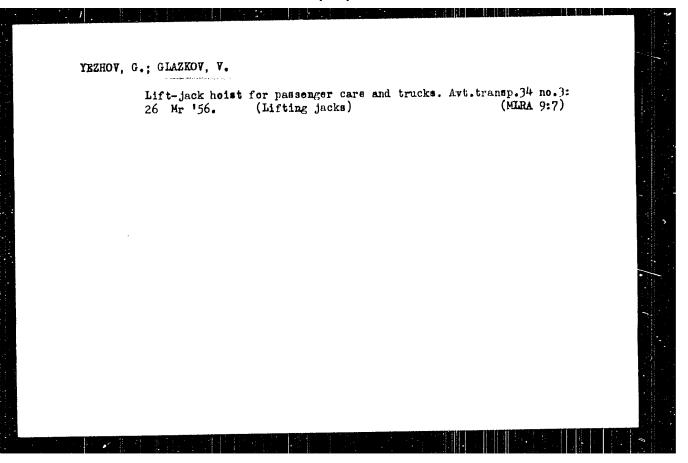
Denniconne, M.M.: GIAPROV, P.N., nauchnyy Botrudnik

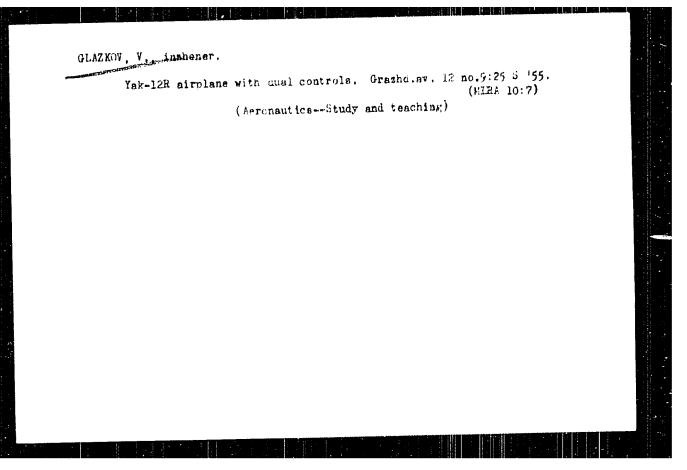
Chemical weed control in Kazakhatan. Tashch. rast. of vred. i
bol. 9 no. 4:3-4 '64. (MEA 17:5)

1. Machallnik Kazakhatanskogo respektikanskogo Pyravleniya
zashchity rasteniy (for Hendarenko). P. Laboratoriya perbitsidav
hazakhakogo instituta zashchity rasteniy (for Hendarenko).

"APPROVED FOR RELEASE: 09/24/2001 CIA-RDP86-00513R000500010019-5







GLAZKOV, V., inzhener.

IAK-12M airplane. Grazhd.av. 13 no.3:23 Mr '56. (MLRA 9:7)
(Airplanes)

GLAZKEV,

84-9-23/47

AUTHOR:

Glazkov, V., Engineer

TITLE:

Yak-12A

PERIODICAL: Grazhdanskaya Aviatsiya, 1957, Nr 9, pp. 21-23

ABSTRACT:

The Yek-12M aircraft has been used in air-chemical operations for a considerable period of time, but its capacity and range were limited. crew have improved on this type. Now A. S. Yakovlev and his design The new model will be known as Yak-12A and its serial production is being considered in the very near future. The wing is trapezoid in shape; its area has been decreased by 1.26 square meters. Each half of the wing is composed of front and rear spars, three stringers, 36 ribs and a leading edge airfoil. The rear spar is attached to the front spar at rib Nr 19. Between the front and the rear spar are fuel tanks, with a total capacity of 166 kg. The wing has ailerons, flaps, and an automatic slot consisting of sections, placed between ribs Nrs 19 and 35. Each section of the slot is suspended on three rockers; the central section has a rubber shock-absorber, 9 mm in diameter, which presses the slot toward the wing. The cantilever is attached to the fuselage by means of two butt joints, set up on the front and back spars. In distinct contrast to the Yak-12M, the cantilever of the Yak-12A is

Card: 1/4

84-9-23/47

Yak-12A (cont.)

supported by only one strut and one counter-strut, against two and three, respectively, in the Yak-LEY The skin covering of the wing has also been modified, being supported by two pairs of ribbon bracings, whereas in Yak-12M it is supported by two struts and three pairs of bracings. The elevator and aileron control is also different in the new model: the sticks were replaced by a wheel. The mechanism of the wheel is installed between frames Nr 1 and Nr. 2. Certain changes have also been made inside the cabin. Instruments are placed to give better control. The plane has a new electric fuel gage. The flare is now in the bow of the wing. The old airpressure gages IIBA -954 were replaced by new IIBA -6M gages. The old NO -500 transformer is replaced by the NO -250 type. The -85 heater will be used more efficiently. The 8-inch oil radiator is also new The capacity of the oil tank is 29 liters. The plane can transport three passengers and 40 kg of baggage, or, if used in rescue operations, it can accommodate two patients and a nurse. If used as a freight plane, it can take 250 kg of freight. Its takeoff speed is 80 km/hr; the takeoff run is 153 meters. The rate of climb at full load is 3.6 m/sec, 0.5 m/sec less than in the Yak-12M. The operating ceiling is 4 km. The gain in altitude is best at 130 km/hr, the operational speed at the above ceiling is 116 km/hr. The maximum speed is 215 km/hr, 35 km/hr more than the

Card: 2/4

84-9-23/47

Yak-12A (cont.)

maximum speed of the Yak-124. A table shows the main comparative specifications of the YaK-12A and Yak-12M, based on a 500 km nonstop flight. Loaded weight: 1588 against 1450 kg; weight of the aircraft: 1059 against 1026 kg; service load remains unchanged, amounting to 109 kg (80 kg - pilot, 19 kg - oil, and 10 kg - service equipment); weight of fueland commercial load - 420 kg against 315 kg; fuel supply (including emergency supply for one extra hour) - 133 against 138 kg; the commercial load, amounting to 287 (against 177) kg, is calculated as follows: 3 passengers against two (or 225 kg against 150), 30 kg of luggage (against 20 kg) and 32 kg extra (against 7 kg). The normal cruising speed of the new type is 170 km/hr against 140, the scheduled speed is 155 km/hr against 127. Productivity in ton/km per hour at a 65% load is 29 against 16. Fuel consumption in kg/hr is 31.5 against 28. The practical range, at an opposing wind of 10 km/hr, is from 600-800 km, all this at full load and with an extra hour's fuel supply. The theoretical maximum range is 1070 km. Maxieuverability remains excellent allowing vertical banks up to 35° at a speed of 130-170 km/hr. The optimum gliding speed is 135-140 km/hr. The extent of retraction of the slat does not affect the trim of the aircraft. Landing with a

Card 3/4

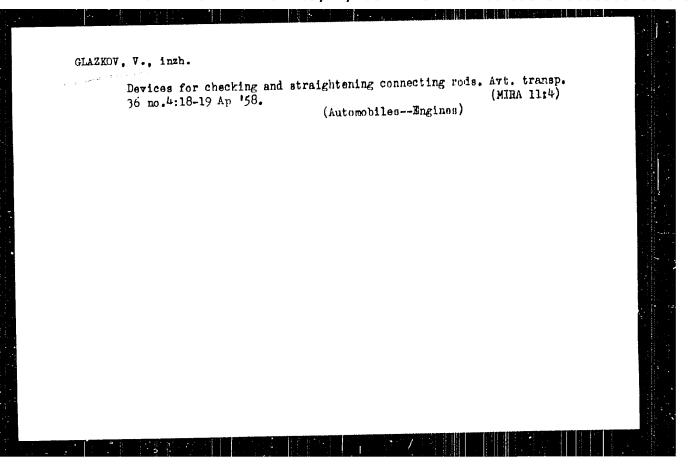
Yak-12A (cont.)

84-9-23/47

40° flap is done at a speed of 90 km/hr. The landing run on a grass surface is 131 meters. The increased cruising speed of the Yak-12A makes the ton/km cost 8 rubles 50 kopeks lower than that of the Yak-12M. A photo and three diagrams accompany this article. The photo shows the new Yak-12A. The diagram on page 22 shows three cross-sectional views of the new plane; the diagram at the topiof page 23 shows an assembly drawing of the Yak-12A; the diagram at the bottom of page 23 shows the comparative maximum speeds of the new and the old Yak-12.

AVAILABLE: Library of Congress

Card 4/4



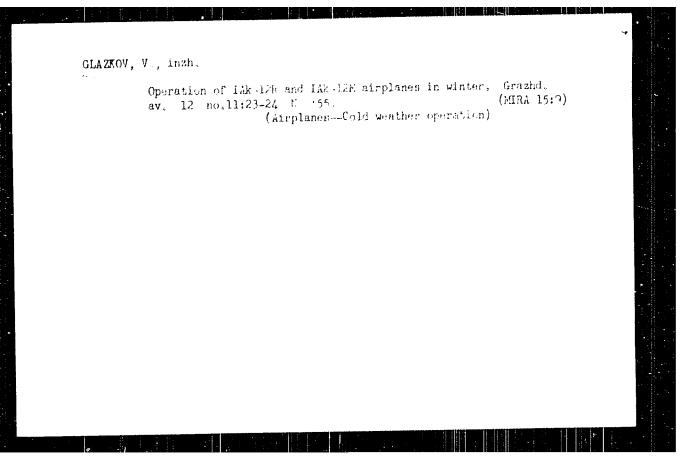
KARTASHOV, G.; GLAZKOV, V.; KUMEKOV, I.

Our suggestions. Prof.-tekh. obr. 17 no.7:17-18 Jl '60.

(HIRA 13:8)

1. Direktor uchilishcha mekhanizatsii sel'skogo khonyaystva No.1
(Stalingradskaya oblast'). 2. Zamestitel' direktora po uchebnoproisvodstvennoy rabote (for Glazkov). 3. Zaveduyushchiy pedagogicheskim kahinetom (for Kumekov).

(Farm mechanization-Study and teaching)



L 10514-63

ACCESSION NR: AP3000729

8/0084/63/000/005/0010/0011

14

AUTHOR: Glazkov, V. (Engineer)

TITLE: Particulars of operation

SOURCE: Grazhdanskaya aviatsiya, no. 5, 1963, 10-11

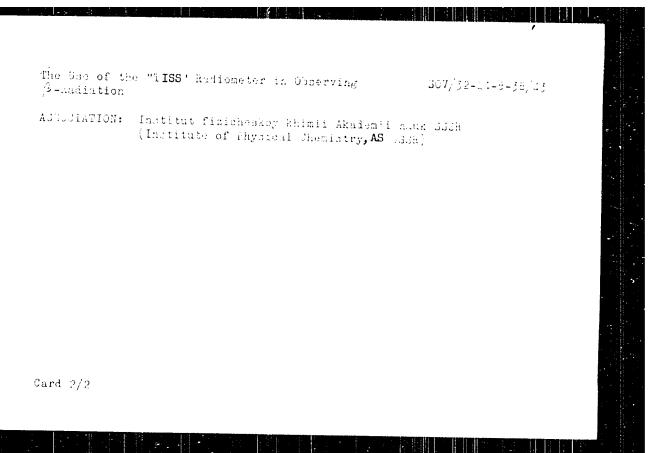
TOPIC TAGS: An-24 turboprop, I1-14, I1-12, I1-2, An-24

ABSTRACT: The An-24 turboprop, which is intended for short- and madium-range flights, has excellent characteristics for local airports with small sirfields and unpaved runways. The II-14, II-12, and II-2 aircraft are being replaced by turboprop planes on interrepublic and interoblast flights and eventually will be replaced on intraoblast air routes. Table 1 of Enclosure compares saveral characteristics of the An-24 and the piston-engine II-14. Orig. art. has: 4 figures

ASSOCIATION: none

Card 1/8/

AUTHORU:	Glaskov, 4- x., Kozoch rov, F. J. S. 1/32-21-8-38/45
TITUS:	The Use of the "TISS" dualog ter in Observing β -madiation (Trimenenty: radiometra ".ISS" dl. a ornarumanty: β - izluchentya)
, ERIODIU, L:	Zavodskaya Laboratersja, 1968, Vol. 34, Nr 8, pp. 1055-1055 (833%)
0.2028A071	This radiometer can be used to observe the soft 5-rays from such isotopes as \$25, 51%, ect. To do this, however, a supplementary unit of measurement must be taken with the end-window counter, as is done with the "I'A" radiometer. For this additional measurement a multiple-core cable is added to the apparatus. A photograph and a schematic diagram of the additional measuring apparatus is given. It is cylindrical in form and consists of two parts which are made of strong steel 1 mm thick and are screwed together. In this case the end-winter statute of the common in the used when low voltage (halomens) or high voltage is desired. There are 2 figures.



107/120-59-4-48/50

· AUTHORS: Mikheyev, N. B. and Glazkov, V. A.

TITLE: A Laboratory Cryostat

PERIODICAL: Pribory i tekhnika eksperimenta, 1959, Nr 4 p 158 (USSR)

ABSTRACT: Soviet cryestates are usually rather bulsy and may not be always easily available. The present note describes construction of a cryostat for temperatures down to -40°C which can be easily prepared in a laboratory possessing a Heppler ultravhermostat or TS-15. Fig. 1 shows schematically the working principle of the cryostat. The ultrathermostat should be fitted with a contact thermometer for low temperatures, and it is connected to a cull of an electromagnetic valve, instead of to a heater. At temperatures higher than the required (set) temperature, the valve is open and the liquid (acetone) sirculates freely between the thermostat and a refrigerator. The liquid is kept in motion by a centrifugal pump of the ultrathermostat. When the required temperature is reached the contact thermometer circuit is broken and the electromagnetic valve is closed by means of a relay;

Card 1/3

357/11:3-53-4-43/50

A Laboratory Cryostat

this stops the circulation of the liquid. When the liquid warms up in the thermostat the electromagnetic valve opens and the whole cycle is repeated. A cylindrical vessel with double walls is used as a refrigerator. This cylinder is made of galvanized iron and its dimensions are: 200 mm external diameter, 150 mm internal diameter, and 250 mm height. To insulate the cylinder thermally it was placed in a wooden box filled with sawdust. The cylinder was filled with acetone cooled with dry ice. The electromagnetic valve (Fig 2) is made of molybdenum glass. The inner (moving) part of the valve is a glass cylinder whose lower conical end fits the outer part of the valve. The interior of this glass cylinder is filled with annealed iron wire impregnated with BF-2 glue solution. When a sugrent passes through the electromagnet coil outside the valve, the iron-filled cylinder is pushed down and this steps the flow of acetone. The electromagnet coil is designed to take 220 V, which is the working voltage of the ultrathermostat. Experimental tests of the cryostat showed that it works down to -300C, holding the temperature constant to within ±0.05°C. To accelerate cooling, dry ice may be placed bown in the refrigerator and Card 2/3 in the cooling liquid of the thermostat. To cool the cryostat

307/12/7-59-4-48/50

A Laboratory Cryostat

from +20°C to -15°C requires 30-40 min. The amount of dry ice required, including the initial cooling of the liquid, is 10-12 kg for six hours work in the region of -10 to -15°C. Note. This is a slightly approach translation. There are 2 figures.

ASSOCIATION: Institut fisioheakov harti Ale 2008 (Paveical Chemistry Institute; Academy of Sciences, USSR)

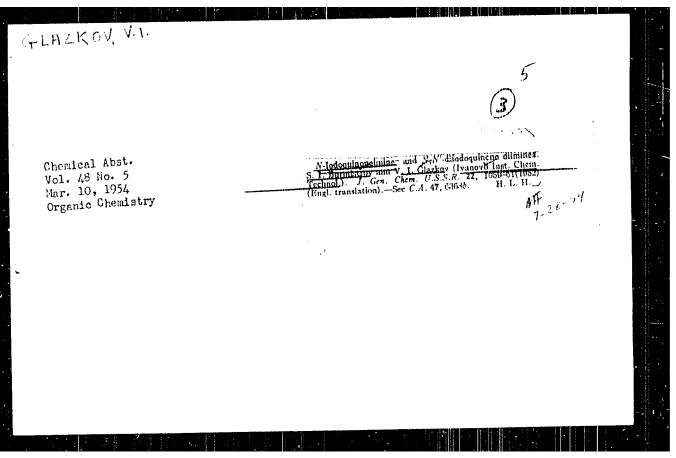
SUBMITTED: July 15, 1190.

Card 3/3

BURMISTROV, S.I.; GLAZKOV, V.I.

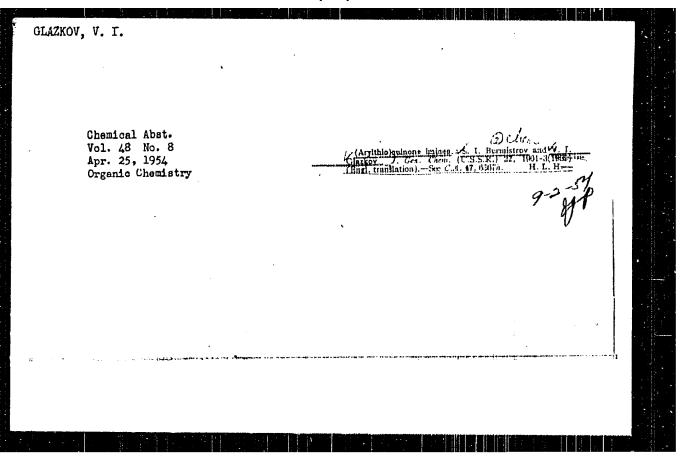
N-Iodoquinoneimines and N.H'-diiodoquinone diimines. Zhur, Obahchey
Ehim. 22, 1004-7 '52.
(CA 47 no.13:6568 '53)

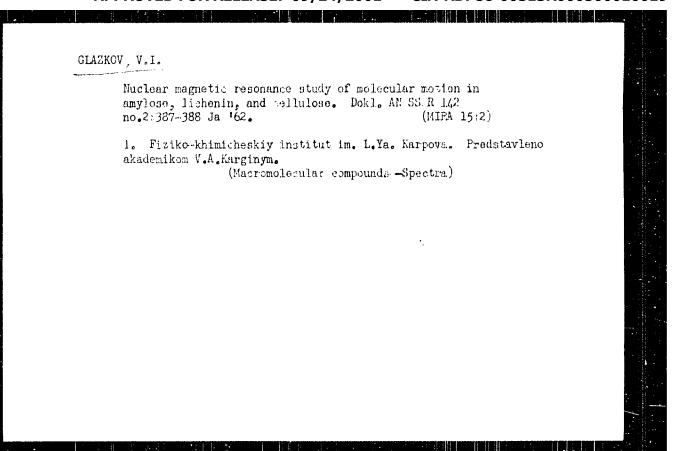
1. Ivanovsk Chem. Tech. Inst.



- 1. BURMISTROY, U. I. and GLAZKOY, V. I.
- 2. USSR (600)
- 4. Imines
- 7. Aryoulfidylquinone imines. Zhur. ob. khim. 22 no. 10. 1952 ~ p-(86)

9. Monthly List of Russian Accessions, Library of Congress, Yobrwary 1953, Unclassified.





GLAZKOV, V.I.

Effect of crystallinity, chain branching, and water content on the shape of the nuclear magnetic resonance line of polysaccharides. Vysokom.soed. 5 no.1:120-122 Ja '63.

(MIRA 16:1)

1. Fiziko-khimicheskiy institut im. L.Ya.Karpova.

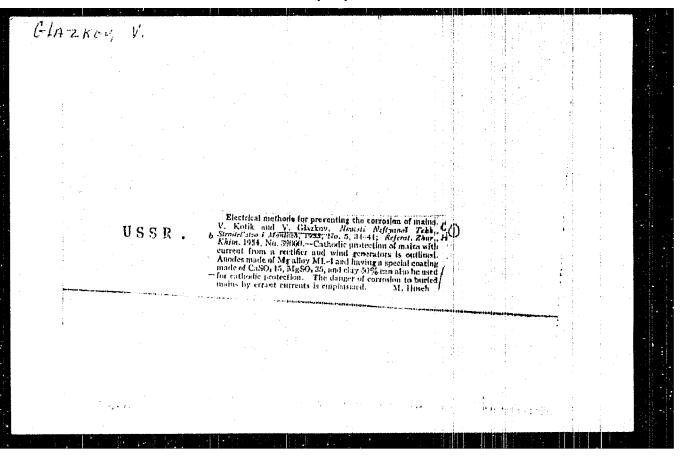
(Polysaccharides--Spectra)

GLAZKOV, V. I.

"Interaction Between the Circuits of Combined Cables." Sub 27 Mar 47. Moscow Inst of Communication Engineers

Dissertations presented for degrees in science and engineering in Moscow in 1947

SO: Sum No. 457, 18 Apr 55



DOI OSHMNKO, P.G.; QLAZKOV, V.I., redaktor; HARTYNOVA, M.P., vedushchiy redaktor; TROFINOV, A.V., tekhnicheskiy redaktor

[Manual on electric measurements and protection of pipelines from corrosion caused by vagrant currents] Rukovodstvo po elektricheskim izmereniiam i zashchite truboprovodov ot korrozii, vyzyvaemoi bluzhdaiushchimi tokami. Moskva, Gos.nauchno-tekhn. izd-vo neftienoi i gorno-toplivnoi lit-ry, 1956. 41 p. (NLRA 9:7)

1. Vsesoyuznyy nauchno-issledovatel'skiy institut po stroitel'stvu VNIIStroineft'.

(Electric currents, Vagrant) (Electrolytic corrosion)

GLAZKOV, V.I., inzhener (Meskva); KOTIK, V.G., inzhener (Meskva)

Cathedic protection station with a semiconducting thermoelectric generator. Strei.prod.meft.prom.l no.5:7-10 J1 '56. (MLRA 9:9)

(Electrolytic corresion) (Petroleum--Pipelines--Cerresion)

CIA-RDP86-00513R000500010019-5 "APPROVED FOR RELEASE: 09/24/2001

Charles and the 118-2-3592 Translation from: Referativnyy Zhurnal, Elektrotekonika, 1957,

Nr 2, p.157 (USSR)

Glazkov, V.I., Kotik, V.G., Doroshenko, P.V. AUTHOR:

Experience in Electrically Protecting Main Pipe Lines from Soil Corrosion (Opyt primenelya elektrozashchity TITLE:

magistral'nykh truboprovodov ot podzemnoy korrozii)

PERIODICAL: Tr. Vses. n.-i. in-ta po str-vu, 1956, Nr 8, pp.97-123

ABSTRACT:

The most effective system is insulation coating combined with electrical protection. The correstveness of the ground is determined by measuring the resistivity of the ground through 50 to 100 m. Those sections of the

Card 1/4

Experience in Electrically Protecting Main Pipe Lines (Cont.)

pipe line most subject to corrosion are likewise determined by measuring the transverse potential gradient. The all purpose YKMH-55 instrument is used in making all electrical measurements on the right of way and on the pipe line. The principal means of protection against soil corrosion are cathode protection installations and other protective installations. When there are local electric networks, rectifiers are used to feed the cathode-protection installations. When there are no local networks, wind-motor or Diesel-generator units are used. These units can be operated periodically to charge storage batteries. Graphite coated and carbon electrodes are used as grounding electrodes at cathode-protection installations.

Card 2/4

112-2-3592 Experience in Electrically Protecting Main Pipe Lines (Cont.)

The electrodes are set up in an activator in order to decrease resistance to current spread. Electrodes from magnesium-base, (M \mathcal{N} -4 and M \mathcal{N} -5) alloys, aluminum or zinc base alloys, or of pure zinc constitute the protective shield. The electrodes are placed 3 to 6 m from the pipe line in an activator (25 per cent magnesium sulfate, 25 per cent calcium sulfate and 50 per cent clay) and are connected to the pipe line. The advantage in using them is that they do not require a source of electric energy. Direct or polarized drainage, cathode protection installations, insulating flanges or electrodes are used to protect pipe lines in stray-current zones. The polarized drainage is designed to conduct a current of 100 to 200 amperes from the pipe line to the rail only. This is done by using polarized relays and mercury interrupters. Due to the possible generation of reverse currents, the use of solid rectifiers or the low-power NBA -39 and PNA -42 drainage units used on underground cables is not recommended. VNII Stroyneft'

Card 3/4

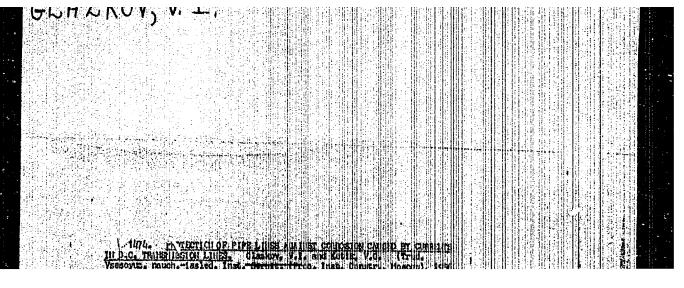
112-2-3592 Experience in Electrically Protecting Main Pipe Lines (Cont.)

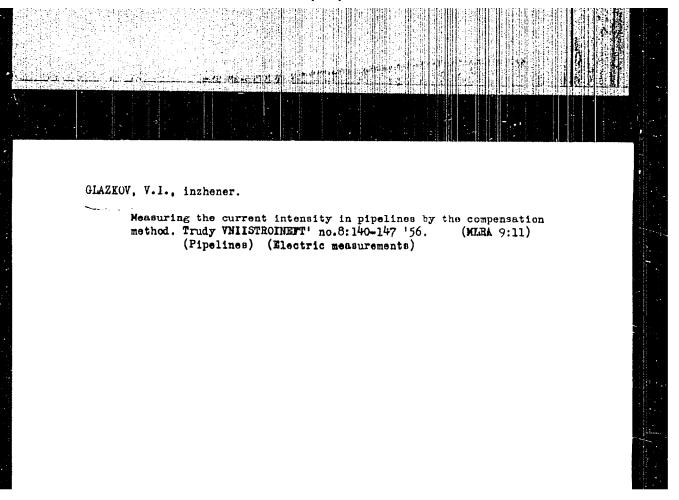
has developed a cathode protection installation which is automatically cut out on the appearance of stray currents and with an excessive increase of negative potential on the pipe line. Protection is improved by reducing the longitudinal resistance of the rail network and by increasing the resistance to current spread (drainage, sleeper impregnation, rubble ballast, reducing the amount of grounded metal equipment connected with the rails.

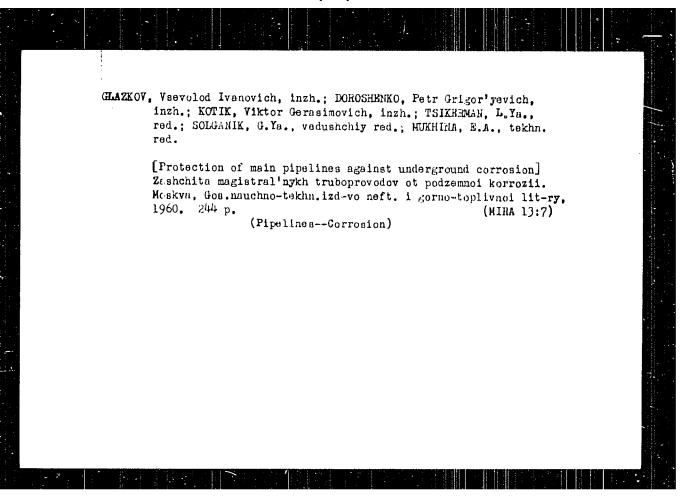
BIBLIOGRAPHY: [Unspecified] eight titles.

D.S.K.

Card 4/4





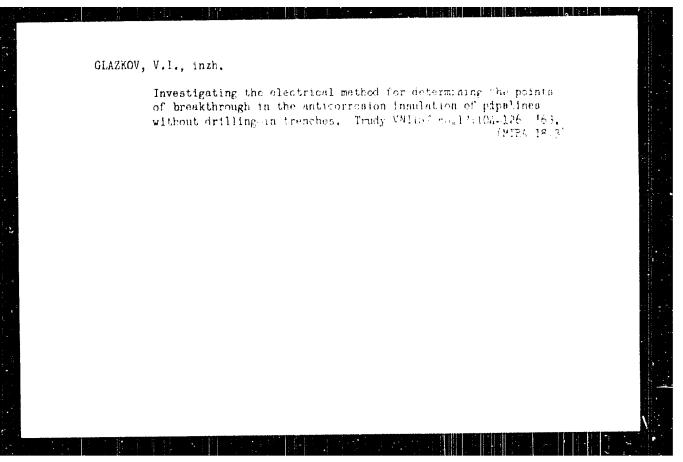


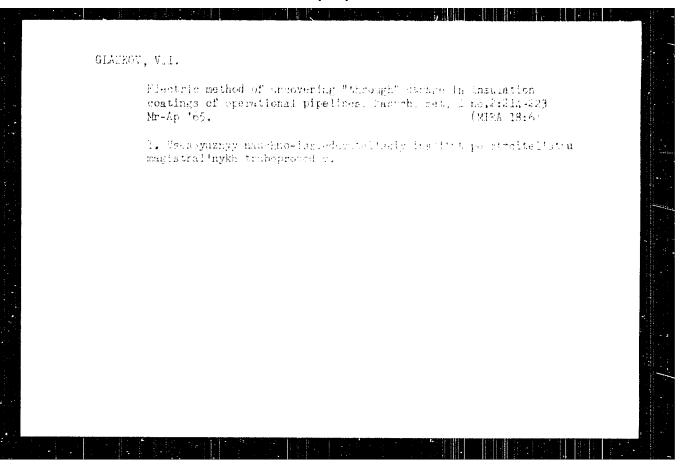
GLAZKOV, V.I., ingh.; ZINEVICH, A.M., ingh.

Inspection of the quality of the insulation of main pipelines.

Stroi.truboprov. 7 no.9:3-6 S 162. (MITA 15:11)

(Pipelines) (Corrosion and anticorresives)





GLAZKOV, V.I.; KOTIK, V.G.

Display at the Exhibition of the Achievements of the Mational Economy of new equipment for the protection of pipelines against electrolytic corrosion. Zashch. met. 1 no.2:254 Mr-Ap '65.

(MIRA 18:6)

KASHCHEYEV, V.H., kand.fiz.-mat. nauk; GLAZKOV, V.M., inzh.

Wear of metals in a flow of abrasive particles of various hardness. Izv.vys.ucheb.zav.; mashinostr. no.8:132-136 '60. (NIRA 13:9)

1. Sibirskiy fiziko-tekhnicheskiy institut. (Nechanical wear)

AUTHORS:

Glazov, V. J. and Borisov, V. A.

TITLE:

A Device for the Automatic Leading of the Specimen in

Measuring Microhardness

PERIODICAL:

Zavodskaya laboratoriya, 1960, Tol. 26, No. 12,

pp. 1420-1422

TEXT: The authors constructed and manufactured a simple device to the apparatus NMT-3 (PMT-3), which warrants the uniform reduction or increase of the diamond gyramid during an exactly determined time when loading or unloading the specimen. Fig. 1 shows the apparatus PMT-5 with the device mentioned. On the main stay of the apparatus, a tracket is fastened, to which, in turn, a controllable notor with a refuser is fitted. The transmission of the rotatory motion from the reducer to the indentor is brought about with the aid of a belt transmission; on the axes of the indentor and of the reducer two special gears are fitted (Fig. 2), which warrant the uniform transmission of the motion. The effect profited by the loading method upon the spread of the results during microhardness tests was studied

Card 1/2

A Device for the Automatic Loading of the Specimen in Measuring Microhardness

\$/032/60/026/012/027/036 B020/B056

on pure aluminum of the type AB-0000 (AV-0000) (99.998% A1). The measured results were statistically evaluated; from these data, the diagrams were drawn (Fig. 3). In automatic loading, the spread of data is much less than in the case of manual loading. The table gives the results of comparative studies, which were carried out on the same aluminum single crystals in the case of manual and automatic loading, using different loads, beginning from 0.5 g. B. Ya. Petrenko is mentioned. There are 3 figures, 1 table, and 2 Soviet references.

ASSOCIATION:

Institut metallurgii im. A. A. Baykova Akademii nauk SSSR (Institute of Metallurgy imeni A. A. Baykov of the Academy of Sciences USSR)

Card 2/2

21321

\$/143/60/000/012/005/007 A163/A026

17 4410

Kashcheyev, V. N., Candidate of Physical and Mathematical

Sciences; Glazkov, V. M., Engineer

TITLE:

AUTHORS:

Comparative resistance to wear of some metals in a flow of

abrasive particles at increased temperatures

PERIODICAL: Energetika, no. 12, 1960, 74 - 77

TEXT: The article deals with the resistance to wear of some metals in a flow of abrasive particles at increased temperatures. The author furnishes data on experimental tests carried out with the following types of steel being used in engineering and boiler construction: 20-type steel subjected to thermal treatment by tempering on laminar and granular perlite; 15 XM (15 KhM), 310 (E10), [13] (G13), X12 (Kh12), CX8 (SKh8M) and 1X18H9T (1Kh18N9T) steels; and BK 20 (VK20) hard alloy. The wearing tests were performed with the help of an installation shown on Figure 1. OKC (OKS) grain, having a hardness of $N_0 \simeq 2,100~{\rm kg/mm}^2$ and a size of 500 - 600 mk, slowly and evenly reached the cylindrical surface of the disc via hopper (1), a

Card 1/5

21,321

Comparative resistance to wear of,

\$/143/60/000/012/005/007 A163/A026

special device (2), and a vertical tube (5). The steel disc (4) rotated at a speed of n=3,500 revolutions per minute. The metals to be tested were fastened into wedge-shaped notches on the circumference of the disc. They had the form of laminae with a cylindrical working surface of 15 x 20 mm. The overall diameter of the disc was 120 mm and the linear speed of the disc rim points 22 m/sec. The disc was set up in an electric furnace (5) lined on the inside to keep the temperature on an even level. The escaping grain was recovered by container (6) and used again, since its abrasive power remained unchanged. The temperature was maintained with the help of \mathcal{M} ATP (LATR) operating with an accuracy of # 100C and fixed with thermocouple (7). The 20-type steel on laminar perlite was tempered at 800°C for 30 minutes and subsequently cooled down at a rate of 15 - 20 degrees per hour by passing the critical points. The tempering on the globular perlite had been carried out at 770° C for minutes with subsequent cooling at a rate of 60-70 degrees per hour. In the course of each test, lasting for 180 - 190, 4 kg of grain was used. The wear of the inserts was determined with an analytical balance and by hydrostatical weighing. The VK20 alloy possesses the best wear-resisting properties, and the 20-type steel, tempered on globular per-

Card 2/5

"APPROVED FOR RELEASE: 09/24/2001 CIA-RDF

CIA-RDP86-00513R000500010019-5

21321 S/143/60/000/012/005/007 A163/A026

Comparative resistance to wear of

lite, the lowest, according to the results obtained. It is interesting to note that, if the initial hardness of the VK20 alloy is about 10 times higher than that of the 20-type steel, the wear of the latter is greater by only 3.6 times at 500°C, and by 5 times at 20°C. In spite of the considerable mechanical differences between the materials selected, the wear of the metals in the abrasive flow did not make them so much different from one another. It may be assumed that the resistance to wear of the 1Kh18N9T, SKh8M and Kh12 steels, and that of the VK2O alloy, is mainly due to their low corrosion at 500°C. In fact, when rotating the disc with the metal pieces at an ambient air temperature of 500°C for 180 minutes without feeding of grains, the weight of the 20-type, 15KhM, E10, and G13 steels decreased by 0.1 - 4.2 mg, that of the Kh12 steel and Vk20 alloy increased by 0.4 - 1.1 mg, and the weight of the SKh8M and 1Kh18N9T steels remained unchanged. The author concludes by pointing out that the highly-manganous G13 steel did not reveal any high wear-resisting properties, although its hardness increased after tempering and cooling during test intervals, while that of other materials decreased. There are 4 figures and 6 Soviet references.

Card 3/5

21321

\$/143/60/000/012/005/007

Comparative resistance to wear of

ASSOCIATION: Sibirskiy fiziko-tekhnicheskiy nauchno-issledovatel'skiy insti-

tut pri Tomskom gosudarstvennom universitete imeni V.V.Kuyby-sheva(Sibrian Physicotechnical Scientific Research Institute

at the Tomsk State University im. V. V. Kuybyshev).

PRESENTED:

at the meeting of the staff members of the Department for the

Physics of Solids

SUBMITTED:

March 8, 1960

Card 4/5

S/145/60/000/008/008/008 D211/D304

AUTHORS:

Kashcheyev, V.N., Candidate of Physico-Mathematical

Sciences, and Glazkov. V.M., Engineer

TITLE:

Wear of metals in a stream of abrasive particles of

various hardness

PERIODICAL:

Izvestiya vysshikh ucnebnykh zavedeniy. Mashinostroye-

niye, no. 8, 1960, 132 - 138

TEXT: The article deals with the resistance to war of commercially pure metals subjected to the impacts of abrasive particles of various hardness. The wear resistance of Pb, Bi, Sn, Sb, Al, Cd, Mg, Zn and steels C60H (S60N) and Ct37 (St37) were investigated using coal, slate, calcite, magnesite and OKC_1 (OKS $_1$) as the abrasive.

The wear of these metals was a function of the hardness of the abrasive, the modulus of elasticity i.e. Young's modulus of the material, and also the coefficient of rigidity of the lattice K. The author states that the wear, expressed in mm³, of metals of various hardness rises sharply if the hardness of the abrasive is comparacand 1/3

Wear of metals in a stream of ...

S/145/60/000/008/008/008 D211/J304

ole with that of the metal. A further increase in the hardness of the abrasive does not lead to an appreciable increase in wear. The wear resistance of metals, expressed as the reciprecal of wear i.e. 1/mm³ in general is directly proportional to the hardness of the metal and also to the magnitude of the interatomic forces. The coefficient of rigidity of the lattice is proportional to the product of the atomic mass m and Debye temperature 0. The wear resistance is a direct function of the product m0. If the wear resistances of the above mentioned metals are plotted in a rectangular system of coordinates, as a function of Young's modulus and the product m0, a graph consisting of a series of straight lines, joined end to end, is obtained. The rate of increase in wear resistance is less steep for softer materials Pb, Bi, Sn, etc. than for harder metals such as Ni, Cu, etc. The mechanism by which the wear takes place when metals are subject to impacts of abrasive particles, is analogous to the process of cutting. The author concludes that an appreciable increase in wear resistance can be achieved if the hardness of the metal is much greater than that of the abrasive. There are 6 figures and 2 tables and 7 Soviet-bloc references.

Card 2/3

Wear of metals in a stream of ... S/145/60/000/008/008/008
ASSOCIATION: Sibirskiy fiziko-tekhnicheskiy institut (Siberian Physico-Technial Institute)
SUBMITTED: February 18, 1960

Card 3/3

21521

10.9230 also 1418, 4016.

S/139/61/000/002/016/018 E073/E535

AUTHORS:

Kashcheyev, V. N. and Glazkov, V. M.

TITLE:

Resistance to Abrasion and the Bond Forces of the

Metal Lattice

PERIODICAL: Izvestiya vysshikh uchebnykh zavedeniy, Fizika,

1961, No.2, pp.156-159

Wear of a metallic surface as a result of impacts by TEXT; abrasive particles on its surface is a recurring problem. Whilst in some cases the aim is to increase the resistance to abrasive wear, in others it may be desirable to increase the abrasive effect of the moving mineral particles. V. D. Kuznetsov and V. N. Kashcheyev (Ref.1) described experiments on the wear of technically pure annealed metals by a flow of abrasive particles carried out for the purpose of determining the relation between the wear resistance, the hardness and the Young modulus of metals. The results did not yield an unequivocal dependence of the wear resistance on the hardness and the Young modulus (data from the literature). However, the graphs show a general tendency of an increase in the resistance to wear with increasing hardness and Card 1/6

21521

Resistance to Abrasion and ...

S/139/61/000/002/016/018 E073/E535

Young modulus. The investigations of M M Khrushchov and M A. Habichev (Refs.2-6) showed that for pure metals in the annealed state there is a direct proportionality between the relative resistance to wear and hardness. Spoor and Newcombe assume that the wear resistance of metals will depend on the elastic properties. According to them, the abrasion wear will be the lower the higher the modulus of elasticity. According to B. M Rovinskiv (Ref.10) a square relation exists between the resistance to abrasive wear and the modulus of elasticity. According to M. M. Khrushchov and M. A. Babichev (Ref.13) the following relation applies to a large number of metals, alloys and minerals in the case of wear by rigidly embedded abrasive grains:

 $\epsilon = const E^{1.3}$

where **t** - relative resistance to wear, E - modulus of elasticity, According to the data of the authors of this paper, the relations governing the destruction of metals by freely hitting abrasive grains differ from those pertaining to embedded abrasive grains. Card 2/6

21521

Resistance to Abrasion and ...

S/139/61/000/002/016/018 E073/E535

Therefore, experiments were carried out for the purpose of establishing a relation between the abrasive wear by means of a stream of abrasive particles and the modulus of elasticity determined directly on the specimens subjected to wear tests. According to K V. Savitskiy (Ref. 15) the resistance of metals and alloys to abrasive wear depends not only on the strength of the interatomic bond but also on the structural state. In the case of considerable temperature rise, the structural factor may be From this point of view metals and alloys which predominant are in the metastable state are of particular interest. It is necessary to assume that only under otherwise equal conditions will the wear resistance be determined unequivocally by the interatomic bond forces. The experiments were carried out with annealed specimens of Pb, Mg, Sb, Bi, Zn, Sn, Cd, Ni, Al, Cu and low carbon (0.04%) steel which were in the form of linings of equal dimensions with cylindrical active surfaces of 13 x 21 mm^2 linings were fixed onto the periphery of a bronze disc of 120 mm diameter. The wear tests were carried out at room temperature by means of a test-rig as shown in Fig.1. A certain charge (3 kg per Card 3/6

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Resistance to Abrasion and ...

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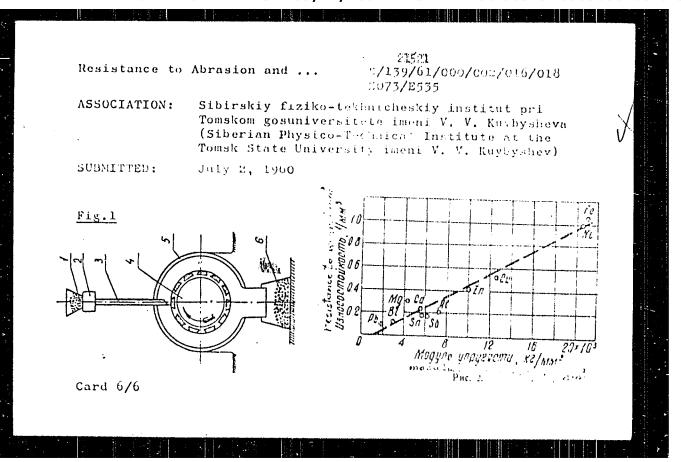
experiment) of abrasive grains of 500-600 u was boured into the bunker 1 and allowed to pass at a slow rate, using a special device 2 with a vibrating needle, through a rectangular cross-section vertical tube from a height of 50 cm,onto a disc rotating at 600 r.p.m. and carrying the specimens under test. The gap between the front wall tip of the tube and the rotating disc was about 4 to 5 times smaller than the average dimension of the used grain, therefore, the air flow which was drawn into the gap could turn the falling grains about their centre of gravity without carrying them away. The slow rate of feeding the abrasive grains was necessary to prevent the bouncing off grains from screening falling grains. The wear of the specimens was determined by weighing with an accuracy of up to 0.1 mg. The bouncing off grains from the internal space 5 were collected in the container 6 and recirculated. The obtained results are plotted in terms of the resistance to wear, 1/mm³, vs. modulus of elasticity, kg/mm² in Fig. 2. Each point represents the average of 5 to 10 experiments, The modulus of elasticity was determined by ultrasonics in the Physics Laboratory of the Tomskiy politekhnicheskiy institut (Tomak Polytechnical Institute), using a device designed by the Card 4/6

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Resistance to Abrasion and ... S/139/61/000/002/016/018 E073/E535

Senior Lecturer A. A. Botaki. The following values of the Young moduli E, kg/mm were obtained: Pb = 1800, Bi = 3000, Mg = $\frac{4330}{5465}$, Sn = $\frac{5640}{5690}$, Sb = $\frac{6090}{5090}$, Al = $\frac{7100}{5090}$, Zi = $\frac{10030}{5090}$, Cu = 12550, Ni = 21220, Fe = 21810. It can be seen that the resistance increases with the Young modulus. The results also show a linear increase in the resistance to abrasion with increasing rigidity, K, of the crystal lattice. Plotting the dependence of K (or the value $m\theta^2$ which is proportional to K) on the elasticity modulus (experimental values), it can be seen that the relation between these is reasonably linear. The modulus of elasticity and the characteristic temperature are characteristics of the bond forces of the crystal lattice; they show little dependence on the temperature and on the structure, which does not apply to the resistance to wear. Although there is no accurate and unequivocal relation, it can be stated that, senerally speaking, there is a close relation between these values and the resistance to abrasive wear will be the higher the higher the modulus of elasticity or the value of $m\theta^2$. There are 4 figures and 15 references: all Soviet.

Card 5/6



KASHCHEYEV, V.N., kand.fiz.-matom.naul; MAZKOV, V.M., insh.

Mechanism of the destruction of a metallic surface by the free impact of an abrasive particle. Izv.vys.ucheb.zav.; energ. 4 no.4:80-85 Ap 161. (MTRA 14:5)

l. Sibirskiy fiziko-tekhnicheskiy nauchno-issledovatel†skiy institut pri Tomskom universiteteimeni V.V.Kuybysheva. Predstavlena otdelom fiziki tverdogo tela.

(Mechanical wear) (Metals)

KASHCHEYEV, V. N.; GLAZKOV, V. M.

Abrasive wear of prestressed nickel. Fiz. met. i metallowed.
14 no.4:608-612 0 '62. (MIRA 1*:10)

1. Sibinskiy fiziko-tekhnicheskiy nauchno-isfledovatal skiy institut.

(Nickel--Cold working)
(Machanical wear)

GLAZOV, V.M.; CHIZHEVSKAYA, S.N.

Some physical properties of gallium arsenide and indium arsenide in the region of melting and the fluid state. Fix.tver.tela 4 no.7:1841-1845 J1 '62. (MIRA 16:6)

1. Institut metallurgii imeni A.A.Baykova, Moskva. (Gallium arsenide) (Indium arsenide)

WH/JD EWT(m)/EWP(e)/EWP(t)/ETI IJP(c) L 06481-67 SOURCE CODE: UR/0363/66/002/006/0976/0979 ACC NRI AP6028293 AUTHOR: Glazov, V. M.; Krestovníkov, A. N.; Yevseyev, V. A. 13 ORG: Moscow Institute of Steel and Alloys (Moskovskiy institut stali i splavov) TITIE: Study of the thermal emf's of group V chalcogenides in the solid and liquid state SOURCE: AN SSSR. Izvestiya. Neorganicheskiye materialy, v. 2, no. 6, 1966, 976-979 TOPIC TAGS: thermal emf, bismuth compound, antimony compound, telluride, selenide ABSTRACT: The differential thermal emf's of the compounds Bl2Te3, Bl2Se3, Sb2Te3 and Sb2Se3 were studied over a wide temperature range (up to 1000°C) in the solid and lim quid state. A substantial drop in thermal emf on melting was observed; this is attributed to an increase in the carrier concentration and an equalization of the electron and hole mobilities. The magnitude of this drop is decreased by the "anionic" replacement by a lighter element, due to the tendency of the thermal emf to increase in the liquid phase as Te is replaced by Se. It is shown that the sign of the thormal emf of Sb2Se3 and Bi2Se3 changes after superheating in the liquid state. A correlation was observed between the nature of the temperature dependence of the thermal emf and the electrical conductivity in the solid phase at high temperatures in Sb2Te3; this is thought to be due to a decrease in deviations from stoichiometry in the Sb2Te3 phase as the temperature rises. On the whole, data on the thermal emf of the 537.311.33 Card 1/2

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LEVENETS, N.P.; SAMARIN, A.M.; SEMIKIN, I.D.; KAZAKOV, V.E.; BEMBINEK, Ye.I.;

PANYUKHNO, L.G.; SVINOLOBOV, N.P.; AVERIN, S.I.; SMIRNOV, V.M.;

ZELENSKIY, V.D.; LAYKO, B.G.; TISHCHENKO, O.I.; OKHRIMOVICH, B.P.;

DANILOV, A.M.; TISHKOV, Yu.Ya.; PANOV, M.A.; MARKELOV, A.I.;

PETROV, A.K.; VASILEVSKIY, P.A.; PASYUK, K.I.; NESTEROV, V.I.;

KHRUSTAL'KOV, L.A.; GLAZKOV, V.S.; MAKAGON, V.G.; FOMIN, G.G.;

TRISHCHENKO, V.D.; KORZH, V.P.; SUYAROV, D.I.; APSEYEV, A.V.;

PAVLYUCHENKO, A.A.; ZHADAYEV, V.G.; KONDORSKIY, R.I.; MOROZOVA,

I.A.; KOCHETOV, V.V.; PRUZHINER, V.L.; MALEVICH, I.A.;

MALIOVANOV, D.I.; ZAKOVRYASHIN, I.I.; NOVSKIY, I.S.; NOVIKOVA,

V.P.; GRISHIN, K.N.; MOSKOVSKAYA, M.L.; KORNEYEV, B.M.

Inventions. Met. i gornorud. prom. no.3:75-76 My-Je *64. (MIRA 17:10)

L 21819-65 EWT(d) LUP(c)

ACCESSION R: APSOCI685

SY0020/64/158/cci./co33/0036

AUTHOR: Class of finite homomorphisms

SOURCE: A class of finite homomorphisms

SOURCE: AN SSSR. Doklady, v. 158, no. 1, 1964, 33-36

TOPIC TAGS: homomorphism

Abstract: A generalized character is a finite homomorphism whose summatory function S(x) = _____ h(n), where n(n) is a finite homomorphism of

natural order, satisfies the condition S(x) = cc x + O(1), where = cis a constant which is usually complex. A character is said to be principal

if cc \pm 0 and is nonprincipal otherwise.

"APPROVED FOR RELEASE: 09/24/2001 CIA-RDP86-00513R000500010019 Card 1/2 L 2|819-65 ACCESSION NR1 AP5001685

ASSOCIATION: Saratovskiy gosularstvernyy univ

Card 2/2

GLAZKOV, Ye. H.; SKOREYEV, I. K.

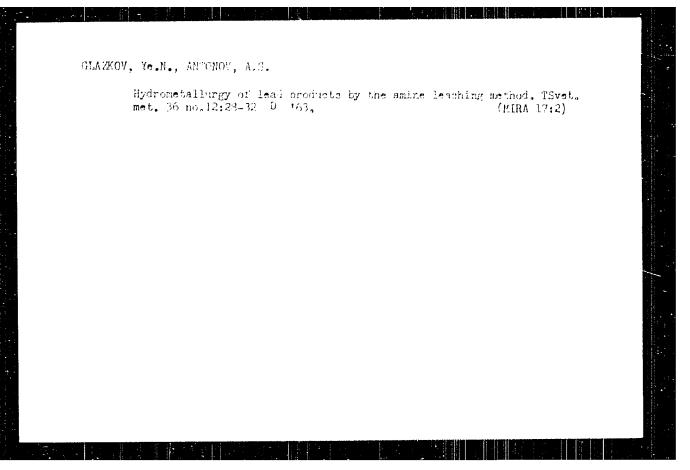
Kinetics of the oxidation of sulfides in a fluidized bad. Trudy Vost. Sib. fil. AN SSSR no.41:145-150 162. (MIRA 15:10)

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(Sulfides-Metallurgy) (Fluidization)

GLAZKOV, YE. N., CAND TECH SCI, "INVESTIGATION OF OXIDIZING ROASTING OF GOLD-BEARING ARSENOPYRITE CONCENTRATES
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SEC SPEC ED RSFSR. IRKUTSK POLYTECH INST. CHAIR OF METALLURGY OF PRECIOUS METALS. IRKUTSK CNKH. [SQVIET OF NATIONAL
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SAMKOV, Ye.A.; CHAZOVA, L.A.; ISXANDEROV, E.M.; DEMIDOV, L.A.; GLIZKOV, Ye.N.

Selectium distribution in the Altya-Topkan mulfuric acid industry. Izv. AR Uz. SSR. Ser. tekh. nauk 9 no.4270-74 '65.

(MIRA 18:10)

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